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APPLICATION NO.	FILING DATE	FIRST NAMED INVENTOR	ATTORNEY DOCKET NO.	CONFIRMATION NO.
10/588,766	08/08/2006	Harald Kraus	4303-1009	2464
<div>465 7590 05/17/2010</div> <div>YOUNG & THOMPSON 209 Madison Street Suite 500 Alexandria, VA 22314</div>				
EXAMINER				
CULBERT, ROBERTS P				
ART UNIT		PAPER NUMBER		
1716				
NOTIFICATION DATE		DELIVERY MODE		
05/17/2010		ELECTRONIC		

Please find below and/or attached an Office communication concerning this application or proceeding.

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APPLICATION NO./ CONTROL NO.	FILING DATE	FIRST NAMED INVENTOR / PATENT IN REEXAMINATION	ATTORNEY DOCKET NO.
10/588,766	8/8/06	KRAUS ET AL.	4303-1009

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ART UNIT	PAPER
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0510

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Commissioner for Patents

The reply brief filed 5/10/10 has been entered and considered.

Applicant has argued that the Examiner has not explained how the velocity (in meters per second) was determined based on the volumetric flow rate (liters per minute) taught by Christenson. However, the Examiner has stated previously (See Non-Final 11/21/08; Final 8/14/09; and Examiners Answer 3/9/10) that Tanaka teaches $d=4\text{mm}$ (d = nozzle diameter) which provides the claimed velocity using a volume flow of minimum 0.1 lpm (liters per minute). For a volume flow of 0.1 lpm the velocity through a 4 mm nozzle would be a velocity of 0.13 m/s which reads on a flow of minimum 0.1 m/s. For a volume flow of 0.5 lpm the velocity would be 0.66 m/s which reads on a flow of minimum 0.1 m/s. In general, the flow rate of a fluid is related to velocity for a given diameter by: $\text{flow rate} = 1/4 * (\pi) * (\text{diameter})^2 * (\text{velocity})$.

Applicant has maintained the argument that Christenson teaches away from the claimed H₂O₂ materials since it is stated that they are highly resistant to dilute etchants. However, the argument has been fully addressed in the Examiners Answer 3/9/10.

/Gregory L. Mills/
Supervisory Patent Examiner, Art Unit 1700
Designee for supplemental answers

/Roberts Culbert/
Primary Examiner, Art Unit 1716